What is the Best Method for Assessing Lower Limb Force-Velocity Relationship?

Abstract

This study determined the concurrent validity and reliability of force, velocity and power measurements provided by accelerometry, linear position transducer and Samozino’s methods, during loaded squat jumps. 17 subjects performed squat jumps on 2 separate occasions in 7 loading conditions (0–60% of the maximal concentric load). Force, velocity and power patterns were averaged over the push-off phase using accelerometry, linear position transducer and a method based on key positions measurements during squat jump, and compared to force plate measurements. Concurrent validity analyses indicated very good agreement with the reference method (CV = 6.4–14.5%). Force, velocity and power patterns correspond to the production of maximal power output [11, 30, 34]. In functional tasks involving a combination of joint rotations, the force-velocity relationship is quasi-linear [2, 5, 28, 35]. Maximal power output is correlated to performance in several sport activities [9, 13]. Likewise, it has been shown that increasing maximal power typically results in improving athletic performance [25, 31]. However, training-induced changes in the force-velocity relationship are subtle in well-trained athletes [4]. Therefore, the assessment of this relationship needs to be really sensitive to any changes in velocity or force output. While many devices and methods have been proposed to evaluate power output during single or multi-joint movements [3, 10, 28, 29], the reference method is based on force plate (FP) data [3, 7]. Recently developed devices (e.g., linear position transducer, accelerometer) or simple methods based on jump height [29] can also be used to assess power output directly at training venue. However, most of these methods have been tested during a single-load (and thus single-
velocity) condition, and no study has investigated their concurrent validity and reliability throughout the whole force-velocity relationship. Therefore, the evaluation of the validity and reliability of the most commonly-used methods would help to accurately monitor training sessions directly on the field and evaluate power output improvement.

The aim of this study was thus to determine the concurrent validity and reliability of the force, velocity and power patterns measured by 3 methods (accelerometer, linear position transducer and Samozino’s methods) during isoinertial vertical jumps.

Methods

Ethics statement
Written informed consent was obtained from each subject prior to participation. This study was approved by the local ethics committee and conducted according to the Declaration of Helsinki. This study meets the ethical standards in sports and exercises science research [17].

Participants
17 volunteers (9 female, 8 male; age: 23.7 ± 3.7 years; height: 171.9 ± 8.6 cm; body mass: 70.2 ± 11.5 kg) participated in this study. This number included 11 sedentary or participants with a low physical activity (i.e., less than 3 h per week) and 6 elite athletes used to squat jumps and testing procedures.

Experimental design
The procedure included 3 test sessions (i.e., familiarisation, test, re-test) separated by 1 week. Participants performed squat jumps with progressive increase in the additional external load to determine their lower limb force-velocity relationship. 3 methods based either on accelerometer, linear position transducer or squat jump positions measurements [29] were compared to a reference method (i.e., force plate). Jumps were executed in a squat rack (Fig. 1a) comprising an anteroposterior and vertical guided bar of 23.6 kg (Max Rack, Gym80 International, Gelsenkirchen, Germany). This system allowed for the execution of free weight-like squats without oscillations in the frontal plane, thus limiting the potential impact of unintended lateral movements on mechanical measurements. A free bar was used for loads under 23.6 kg, and a 0.5 kg bar was used in body weight condition to simulate the same experimental configuration for all tested loads. Pilot data showed that frictional forces were negligible with the guided bar (1.1 ± 0.1 N, i.e., 0.09 ± 0.02% of body mass).

During the familiarization session, the starting position was self-selected by the participant. The position was then kept constant for subsequent trials. A marker on the squat cage indicated the bar height (Fig. 1a) in this position. Then, participants performed squat jumps with load increasing progressively. Participants were asked to jump with the bar (ballistic movement) so that they use the whole range of motion and produce the greatest possible amount of power output [6]. The load increment depended on the jump height achieved during the body weight condition (with a 0.5 kg bar). Under a 0.2 m jump height, 10% of the body mass was added at each trial until the load was sufficient to obtain a jump height below 0.05 m. A supplemental load corresponding to 15, 20, or 25% of body mass was added when jump height in the body weight condition was above 0.2 m, 0.3 m, and 0.4 m, respectively. The maximal additional load the participants were able to lift concentrically once (1RM) was...
determined from the load-velocity relationship obtained during the familiarization session. 1RM was selected as 90% of the load corresponding to zero velocity [23]. During test and re-test sessions, the 7 tested loading conditions were 0, 10, 20, 30, 40, 50 and 60% of 1RM.

At the beginning of each trial, participants were asked to stand still on the force plate to assess the total system load (i.e., participant body mass + external load). After staying in the starting position for 1 s, the participant jumped as fast and high as possible. Participants performed 2 trials at each load, plus a third one in the case of a 10% height difference between the 2 trials. The highest jump trial was considered for further analysis. Movement execution was monitored through the FP signals and trial was repeated if the jump was not executed properly (i.e., if countermovements were observed).

Data collection and processing
For each method, force, velocity and power signals were obtained as follows.

**Force plate**
A force plate (FP) (Kistler, Wintertur, Switzerland) was used as reference method. Vertical ground reaction force was recorded and sampled at 1000 Hz. $F_m$ component was used to calculate the vertical instantaneous acceleration ($a_z$; m·s$^{-2}$) of the centre of mass (COM):

$$a_z = \frac{F_m}{m} - g$$  \hspace{1cm} (1)

where $m$ is the total mass (in kg). $a_z$ was then integrated to provide instantaneous vertical velocity ($v_z$; m·s$^{-1}$) of the COM at time $t$:

$$v_z = \int a_z dt + v_{z0}$$  \hspace{1cm} (2)

As the jump begins with a period of immobility, at $t_0$:

$$v_{z0} = 0$$  \hspace{1cm} (3)

At each instant, power was then calculated as the product of force and velocity ($P_z = F_z \times v_z$; in W).

**Accelerometer**
The 3-dimensional accelerometer (Acc) used in this study was a Myotest Pro (Myotest SA, Sion, Switzerland) that was directly fixed to the bar. Mechanical signals (i.e., force, velocity, power) were recorded at a sampling frequency of 500 Hz. At each instant, acceleration of the bar was used to calculate force:

$$F = a m$$  \hspace{1cm} (4)

Velocity and power were obtained in the same way as for force plate data analyses.

**Linear position transducer**
The linear position transducer (LnT) GymAware (Kinetic Performance, Mitchell, Australia) was tested in this experiment. LnT was composed of an encoded wire directly fixed to the bar and winding into a sensor unit fixed to the floor. The sensor timestamped the displacement data with a 1 ms resolution and then down-sampled to 50 Hz.

Vertical displacement ($d_z$) of the bar was differentiated once to calculate instantaneous velocity ($v_z$). Velocity was then differentiated to calculate instantaneous acceleration. Force and power were obtained in the same way as accelerometer and force plate signal analyses.

**Samozino’s method**
Samozino’s method (Sam) is a simple method based on Newton’s second law, establishing that mean force ($\bar{F}$), velocity ($\bar{v}$), and power ($\bar{P}$) can be calculated during a vertical jump movement from the jump height and squat jump positions measurements [29]. Jump height was obtained using an OptoJump Next optical measurement system (Microgate, Bolzano-Bozen, Italy). Mean force ($\bar{F}$), velocity ($\bar{v}$) and power ($\bar{P}$) were calculated using the following equations:

$$\bar{F} = mg \left( \frac{h_{PO}}{h_{PO} + 1} \right)$$  \hspace{1cm} (5)

$$\bar{v} = \frac{h_{PO}}{t_{PO}}$$  \hspace{1cm} (6)

$$\bar{P} = mg \left( \frac{h_{PO}^2}{h_{PO} + 1} \right) \sqrt{gh}$$  \hspace{1cm} (7)

where $m$ is the body mass of the subject (in kg), $g$ is the gravitational acceleration (in m·s$^{-2}$), $h_{PO}$ is the vertical push-off distance (in m), $t_{PO}$ is the push-off phase duration (in s) and $h$ is the jump height (in m).

Anterior iliac crest was selected as anatomical marker to calculate the vertical push-off distance ($h_{PO}$). The vertical push-off distance corresponded to the displacement of the marker between the starting position and the moment of toe-off. The vertical position of the marker was easily determined with a stadiometer in the starting position. For toe-off moment position, the participant was lying on his back, ankle in maximal extension with tip of toes reaching a wall. The distance between the wall and the iliac crest corresponded to the vertical toe-off position of the marker. These measurements were done and verified at the beginning of each test.

All data were analysed with custom-written scripts (Origin 9.0, OriginLab corporation, USA). The onset of the push-off was set as the point corresponding to a 50 N increase of the vertical force at the end of the stabilization period in the starting position (Fig. 1b). The offset of the push-off phase (i.e., take-off) corresponded to the point where vertical power reached zero (Fig. 1c). For graphical representation standardization, a linear interpolation technique was used to obtain force, velocity and power values every 5% of the total duration of the jump push-off phase [12]. Therefore, the same amount of points was used to represent all movements. The average force, velocity and power were calculated between those onset and offset time points for each loading condition.

**Statistical analyses**
**Sample size**
A non-inferiority sample size calculation was used to determine the sample-size required for the validity analysis. Data for the sample size calculation were collected in a pilot study. Non-inferiority limits were set at 5% of the maximal values obtained in the pilot study (i.e., 135 N for force, 0.06 m·s$^{-1}$ for velocity, 113 W for power), with standard deviations of 371 N for force, 1.18 m·s$^{-1}$ for velocity, and 30 W for power. The sample size was calculated as follows:

$$n = \frac{\left( \frac{\sigma_1}{\sigma_2} \right)^2 \left( \frac{\delta_1}{\delta_2} \right)^2}{4 \left( \frac{\delta_1}{\sigma_1} \right)^2}$$
for velocity, and 317 W for power. Significance and power criteria were set at 5% and 80%, respectively. It was necessary to test 15 participants. We chose to increase the number to 17.

Validity and reliability
To determine the concurrent validity of the different methods, linear regressions were performed and Bravais-Pearson correlation coefficient (r) were determined between FP (i.e., reference measurement) and LnT, Sam, and Acc methods for mean force, mean velocity and mean power. Coefficients of variation (CV) were calculated [20]. The level of concordance for measurements between LnT, Sam, Acc and FP method were assessed using Bland-Altman plots, with limits of agreement defined as the mean difference ± 1.96 SD of the difference [1]. The reliability between the 2 test sessions was evaluated for the mean force, velocity and power, using the intraclass correlation coefficient (ICC) and CV [20].

Results

Force, velocity and power patterns
Fig. 2 displays the patterns of force, velocity and power provided by FP, LnT and Acc during squat jumps performed at 0, 30, and 60% of 1RM. When considering all methods and testing conditions, participants exerted maximal force, velocity and power values of 1695.0 ± 386.8 N (range: 981.5–2764.3 N), 1.50 ± 0.46 m·s⁻¹ (range: 0.75–2.99 m·s⁻¹) and 1413.7 ± 465.7 W (range: 526.0–2718.8 W), respectively. Kinetic patterns of LnT and Acc were slightly different from FP for the 0% of 1RM loading condition. The time occurrence of the maximal force changed depending on the method (i.e., between 50% and 60% of the push-off phase), while in the heaviest loads maximal force occurred at the same instant of the push-off (i.e., 65%) for all methods.

Validity of mean parameters
Pearson correlation coefficients were 0.98 for force for all tested methods, were lower for velocity than for force (for FP vs. LnT, r = 0.91; FP vs. Acc, r = 0.87; FP vs. Sam r = 0.88) and lower than 0.90 for power (LnT and Sam, r = 0.89; Acc, r = 0.87). CV were lower than 5% for force (LnT, CV = 3.3%; Acc, CV = 4.2%; Sam, CV = 3.7%). Velocity CV ranged from 6.4% for LnT to 11.4% for Sam, and reached 8.2% for Acc. CV were lower than 15% for power measurements (LnT, CV = 14.5%; Acc, CV = 12.5%; Sam CV = 13.3%).

Reliability of mean parameters
Mean ICC and CV for average force, velocity and power recorded with FP, LnT, Acc and Sam methods are shown in Table 1. The results demonstrated an excellent reliability for the 3 parameters with ICC ranging from 0.89 to 0.99. Force measurements showed CV values lower than 5% for all methods. CV values were lower than 10% for velocity, except for Acc (CV = 10.2%), CV were slightly higher than 10% for power except for Sam (CV = 8.6%).

Discussion
The present study aimed to evaluate the concurrent validity and reliability of the methods most commonly used to determine average force, velocity and power during the push-off phase of vertical loaded jumps. Slight differences were observed between the tested methods and force plate measurements for high velocity and power levels. Overall, our results indicate that force, velocity and power measurements can be assessed with the present methods, as they all presented similar validity (Fig. 3), while measurements obtained from the Samozino’s method showed the most reliable results.
To our knowledge, this study is the first to compare the current available methods used for the assessment of the force-velocity relationship of the lower limb extensor muscles. Linear position transducer and accelerometer allow for the description of the entire time-course of mechanical parameters recorded during the jump push-off phase (Fig. 2). The comparison of force, velocity and power patterns obtained with those methods exhibited almost perfectly overlapped curves compared to the reference method (force plate). However, the validity of mechanical measurements decreased as velocity increased (i.e., near body weight condition, Fig. 2). The position measurements performed with the transducer consider the movement velocity when the encoded wire is winding into the sensor box. Indeed, as the velocity increases, the sampling frequency increases thus leading to more accurate measurements. Moreover, it has been shown that the measurements obtained with accelerometry are more valid as acceleration is higher (i.e., high velocity movement). Therefore, the variability of measurements performed during high-velocity jumps cannot be attributed to devices limitations [22]. This finding has been observed in previous investigations that used identical linear transducer and accelerometer, which showed a weaker agreement for mechanical measurements obtained during fast movements [7]. These results could originate from the fact that light loading/high-velocity conditions could influence the jump trajectory notably by intensifying non-vertical movements and probably accentuate the differences between methods. A guided bar would possibly have been able to limit this phenomenon in high-velocity conditions. This observation suggests more valid mechanical measurements during slower movements (i.e., heavier loads). Actually, the comparison between the tested methods and the reference revealed slight differences (when considering all load conditions) especially for mean velocity and power data (Fig. 2). As previously reported, these differences could be due to the fact that linear transducers and accelerometers evaluate the bar dis-

![Fig. 3 Bland-Altman plots of force plate (FP) vs. linear position transducer (LnT, top panel) accelerometer (Acc, middle horizontal panel), and Samozino’s method (Sam, bottom panel) for force (left panel), velocity (middle vertical panel) and power (right panel) measurements. Bias and 95% confidence interval (CI) are indicated for each plot.](image)

<table>
<thead>
<tr>
<th>Force (N)</th>
<th>FP</th>
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<th>Acc</th>
<th>Sam</th>
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patterns (i.e., rate of force or power development) changed as the shape of mechanical variations that should be observed through the push-off phase of a squat jump performed under different loading conditions. Furthermore, while all methods are reliable, the Samozino’s procedure provides the greatest reliability. Those methods permit between-session comparison and characterization of the training-induced effects. While mechanical patterns appear to differ from one method to another, especially when light loads are involved (i.e., high velocity), these methods can be used with confidence to assess the force-velocity relationship and provide information on the athletic profiles of trained and untrained subjects. Our findings and the ease of use of the Samozino’s procedure suggest that this method is suitable for monitoring power training sessions under field conditions.

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